In -situ, High Temperature Study of Phase Transformations in Ceramics

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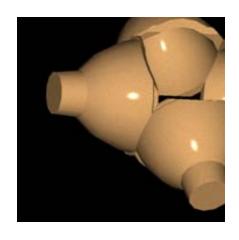


Goal of this work

- To explore the feasibility of using the thermal-image technique to study reversible, displacive-type phase transformations, specifically in air, at elevated temperatures
- ➤ To measure their lattice parameters as a function of temperature and determine their axial thermal expansion coefficients, transformation temperatures and unit cell volume/shape changes

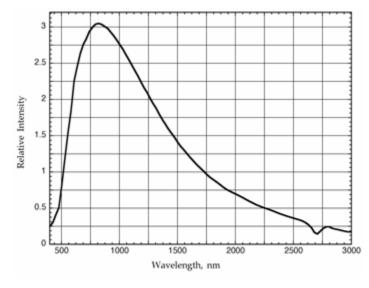


Halogen lamp





Osram Xenophot HLX 64635 15V 150W

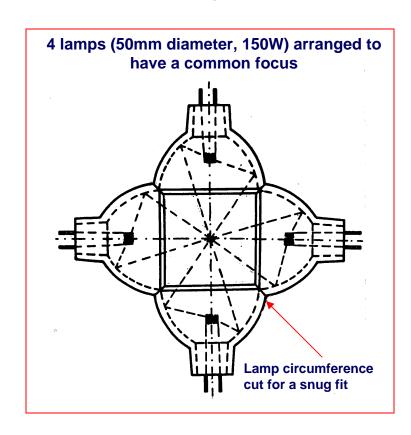


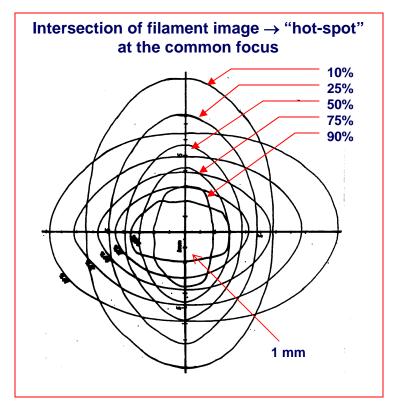
Radiation of the halogen lamp



A Compact Thermal-image Furnace

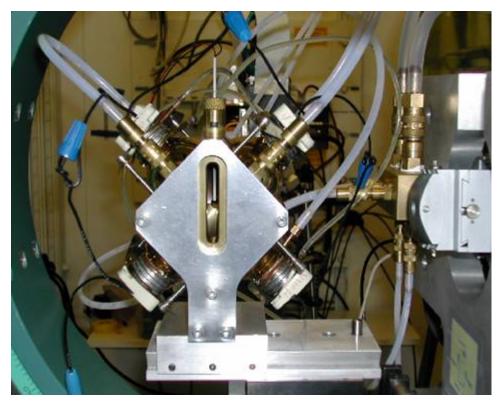
Heat source: halogen infrared reflector lamp (OSRAM Xenophot HLX64635)







High Temperature Furnace



Setup at UNICAT beamline 33BM at APS; Argonne National Laboratory

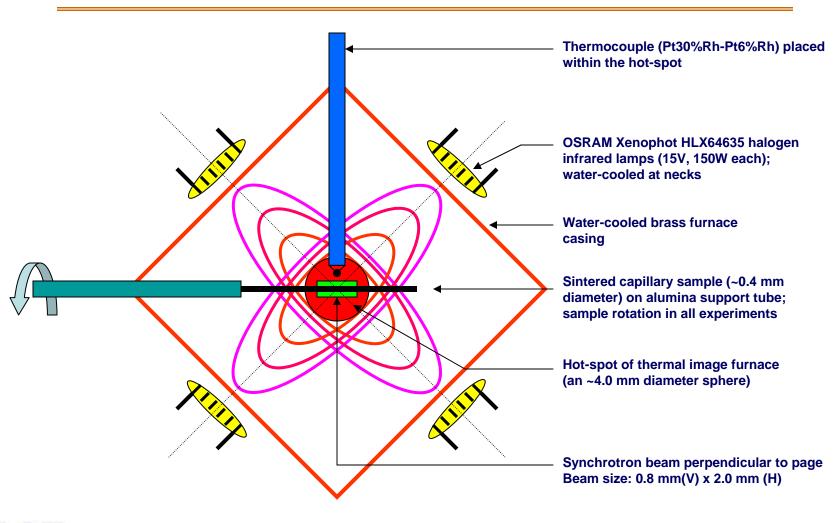
Water cooling

Goniometer for specimen rotation

Thermocouple

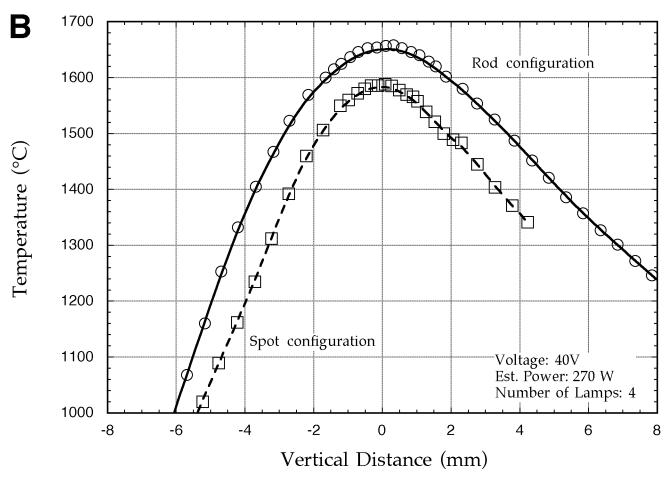


Layout



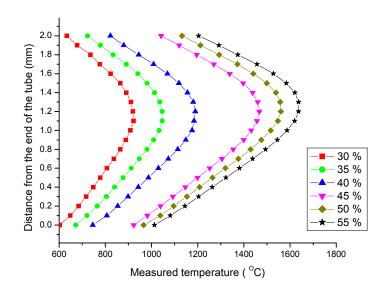


Temperature Profile of Quadrupole (at 2/3 power)

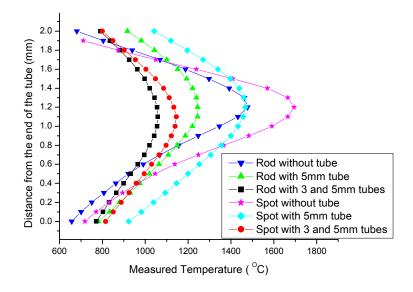




Temperature measurement



Temperature measurement Hot spot with Al_2O_3 tube (OD: 5 mm, ID: 4 mm)

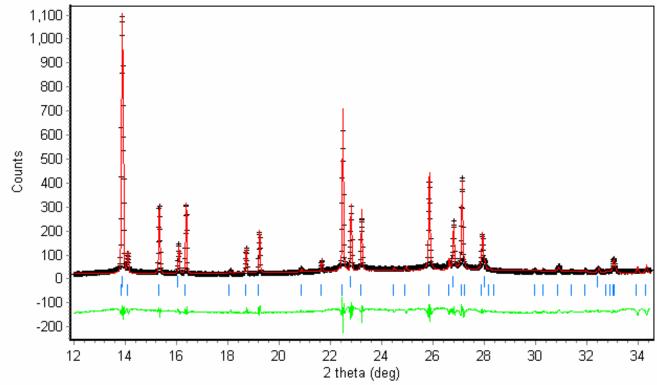


Temperature measurement with change of lamp and tubes



In-situ HTPXRD: $RNbO_4$ (R = Dy, Y)





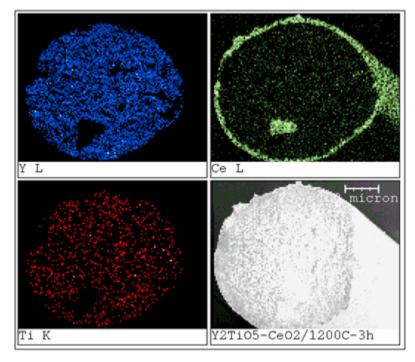
Obvious TDS indicating attainment of very high temperatures *insitu* in air in this work



Preparation of Capillary Sample

- Powder preparation
 - PVA method
 - ethylene glycol method
- Capillary fabrication
 - extrusion
 - "controlled" sintering
- "Thermometer" coating
 - platinum ink
 - oxide layer

(CeO₂ mp: 2300°C, MgO mp: 2800°C)



A representative capillary sample (diameter ~0.35 – 0.40 mm)



Temperature Calibration

Up to 1700 °C

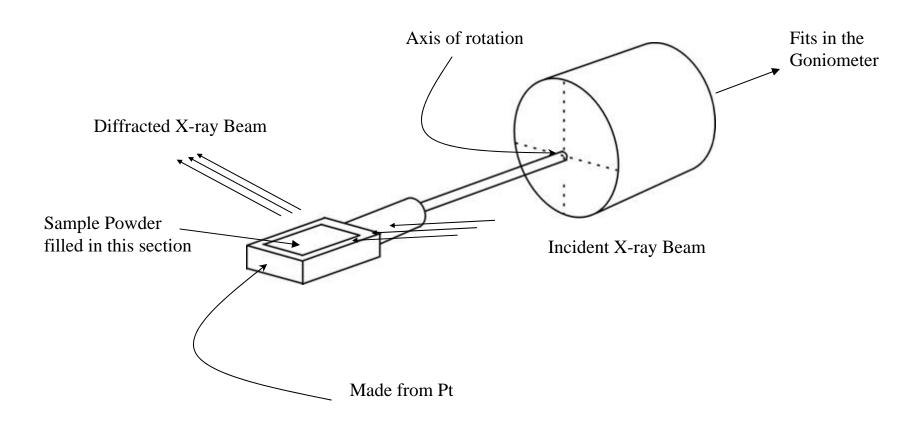
- Thermocouple Pt 30% Rh Pt 6% Rh in close proximity to specimen
- Accuracy ±10 °C at 1500 °C

Above 1700 °C

- Lattice constant of coating material
- Furnace power calibration with known melting points and phase transformations
- Accuracy ±30 °C at 2000 °C



Reflection Geometry for *in-situ* high temperature phase transformation studies at UNICAT 33BM Beam line at APS





Advantages

- In situ studies of lattice parameter development and phase transformations possible up to 2000 °C
- In air studies
- Quick temperature ramping
- Easy sample preparation



Problems

Temperature calibration

- Insufficient known calibration materials
- Thermal expansion mismatch between coating and specimen
- Reaction between calibration material and specimen under study

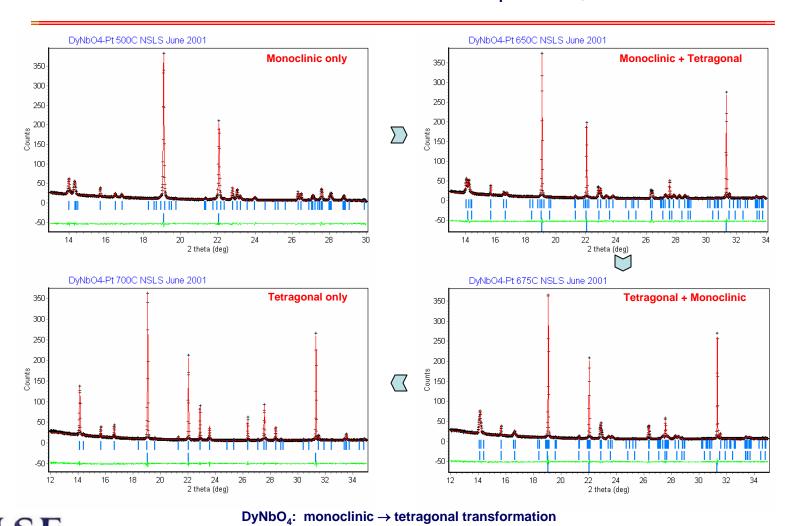
Specimen stability

- Structural (specimen disintegrating, glassy phase)
- Chemical stability

X-ray absorption by heavy elements in Debye-Scherrer geometry Thermal expansion of sample holder in Bragg-Brentano geometry



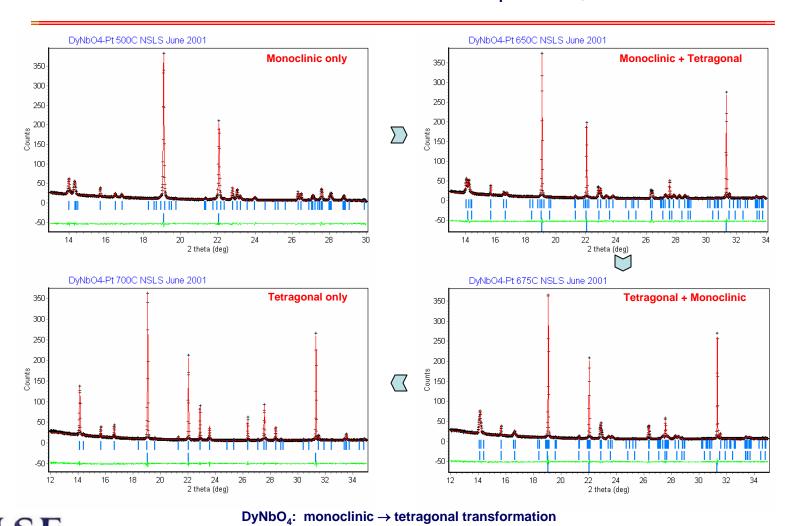
In-situ HTPXRD in Air: $RNbO_4$ (R = Dy, Y)



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In-situ HTPXRD in Air: $RNbO_4$ (R = Dy, Y)

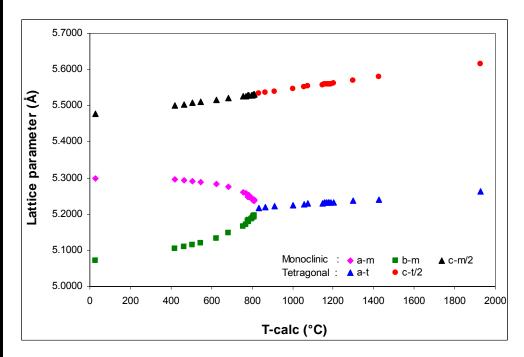


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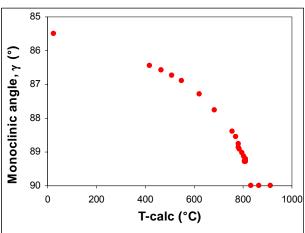
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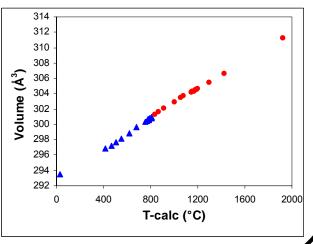
In-situ HTPXRD in Air: RNbO₄ (R = Dy, Y)

YNbO₄: monoclinic-to-tetragonal transformation



Temperature evolution of a, b, c, γ and unit cell volumes





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Conclusion for LnNbO₄

- the monoclinic-to-tetragonal transformation
 - in YNbO₄ is 2nd order at ~830 °C
 - the room temperature spontaneous strain of YNbO₄ is
 6.35%



Compound	<u>Crystal</u> <u>Symme tries</u>	Transformation Temperature (To on cooling)	<u>Volume</u> <u>Change (ΔV)</u>	<u>Unit Cell</u> Shape Change(°)
ZrO2	Tetragonal → monoclinic	950	(+)4.9% (R.T.)	9
Ln2O3 (type)	monoclinic → cubic	600—2200	(+)10%	10
Ca2 SiO4 (K2SO4-type)	monoclinic → orthorhom bic	490	(+)12%	4.6
Sr2SiO4 (K2SO4-type)	orth or hom bic →mo noclinic	90	0.2%	2
NiS	rhom boh edr al → hexagona l	379	(+)4%	-
2Tb2O3.Al2O3 (type)	orth or hom bic →mo noclinic	1070	(+)0.67%	18.83
PbTiO3	cubic → tetragonal	445	(+)1%	0
KNb O3	tetra gon al → orth or hom bic	225	~0%	0
LuBO3	hexagona l → rhom boh edr al	1310	(+)8%	-
MgSiO3 (CaSiO3-type) (FeSiO3-type)	orth or hom bic →monoclinic	865	(-)5.5%	18.3
YNb O4 (Ln Nb O4-ty pe)	tetra gon al →mo n oclinic	900	(-) 1.8%	4.53
LnBO3 (type)	hexagona l→ hexagona l	550—800	(-)8.2%	-





Compound	<u>Crystal</u> <u>Symmetries</u>	Transformation Temperature (To on cooling)	Volume Change (ΔV)	<u>Unit Cell</u> <u>Shape</u> <u>Change(°)</u>
Cristobalite (SiO2)	cubic → tetragonal	265	(-) 2.8%	0
Hexacelcian (BaAl2Si2O8)	hexagonal → orthorhombic	300	(-) 0.43%	0
Leucite (KAISi2O6)	cubic → tetragonal	620	~0	0
Zircon (ZrSiO4)	monoclinic → tetragonal	827	?	?
Di-lanthanide aluminates (Ln4Al2O9)	monoclinic → monoclinic	1400	(+) 0.5%	?
Di-lanthanide titantes (Ln2TiO5)	hexagonal → orthorhombic	1712	?	0
Barium orthotitanate (Ba2TiO4)	?	?	?	?
Cerium pyrosilicate (CeSiO4)	?	?	?	?
Aluminum titanate (Al2TiO5)	?	?	?	?
Lithium phosphate (Li2PO4)	?	340	?	?
Lanthanide (eg.Gd) vanadates (LnVO4)	monoclinic → tetragonal	825	?	?

Table 2. Other Examples of Phase Transformations in Ceramics

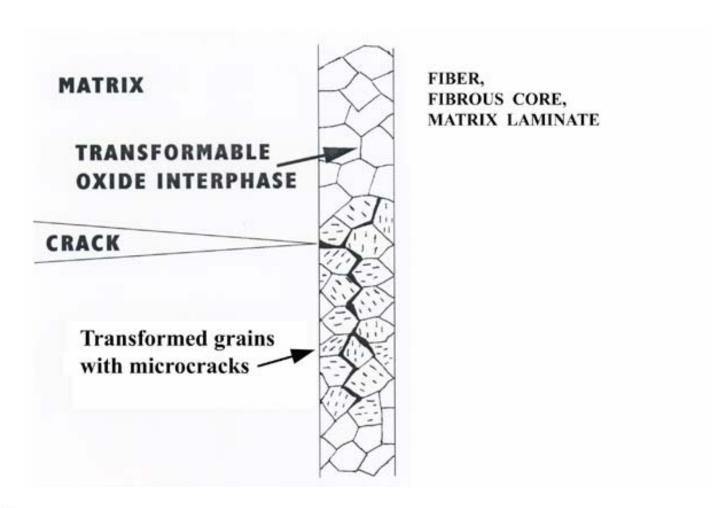


Table 3. RARE-EARTH OXIDES: PHASE TRANSFORMATIONS

Compound	La	Се	Pr	Nd	Pm	Sm	Eu	Gd	Tb	Dy	Но	Er	Tm	Yb
LnNbO₄ scheelite	Monoclinic (low T) → Tetragonal (high T)													
Ln₂TiO₅	Orthorhombic					Orthorhombic (low T) → Hexagonal → Cubic					Cubic			
LnAlO₃ Perovskite	Rhombohedral (low T) → Cubic			(low orthorh	ohedral T) → nombic ubic	(lo	bohedra w T) → rhombio		Orthorhombic					
LnTaO₄	Unknown Monoclinic (I					low T) → Tetragonal				Monoclinic				
LnVO₄	Мо	noclinic (?)												
LnAsO₄						YPO₄ structure I scheelite (CaWO₄) structure (high pressure)								
LnPO₄	Monoclinic CePO₄ structur					Tetragonal YPO ₄ structure					ıre			
Ln ₂ Ti ₂ O ₇	Cubic (Monoclinic						pyro	pyrochlore)						
Ln₃NbO ₇	7	Гetragon	al (?)	?			He	kagor	agonal			?	



Toughening of Ceramics by Transformation Weakening of Interphases



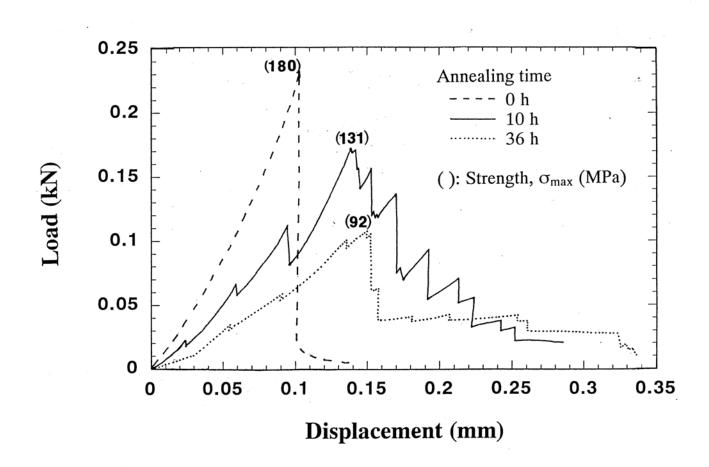


Toughening Mechanism

- Schematic diagram illustrates "transformation weakening of ceramic interphases" leading to overall toughening of a ceramic matrix composite.
- In thermally induced transformations, all interphases are pretransformed before the approach of a crack, with some consequent loss of overall strength of the material.
- In the ideal, shear-stress induced case, an oncoming crack induces a transformation in its immediate environment, with strength only minimally reduced throughout the bulk.
- Maximum toughening is achieved, since the propagating crack needs to do work to overcome the nucleation barrier and cause transformation, and onset of the other synergistic toughening mechanisms (e.g., crack formation) occurs.

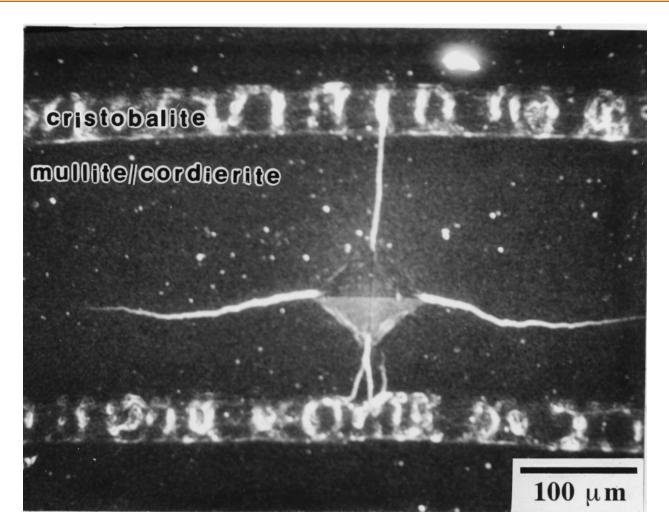


Work of Fracture of TW Weakened Composite



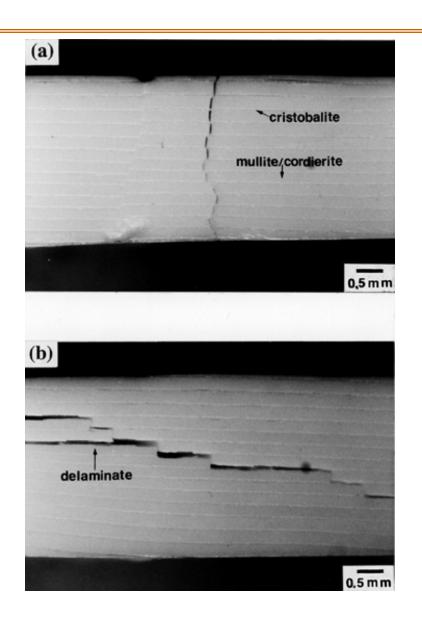


Preferential Crack Deflection along TW Interphases





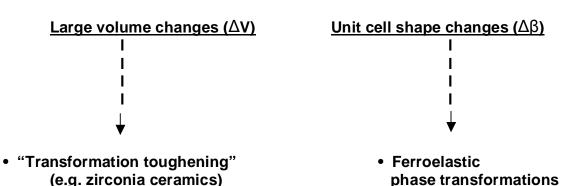
Toughening by TW of Interphases





Long term vision for study of phase transformations in structural ceramics and composites

Displacive phase transformations can be accompanied by volume changes and/or by shape changes



- "Transformation weakening" of interphases, giving overall toughening of fiber-reinforced composites or fibrous monoliths (e.g. enstatite, cristobalite)
- Toughening by

Ferroelasticity



"twin filipping"

Structural ceramics for airplane and

Ground-based turbine engines

Large force actuation (e.g., for MEMS devices) Shape memory ceramics

